

Post Tensioning Awards 2009



Project Summary

Type of structure	Residential with leisure suites including Swimming pool, Cinema, Virtual Golf, Wine Cellars, and Parking accessed via 2 car lifts
Location	Knightsbridge, London
Architects	Roger Stirk Harbour + Partners
Structural Engineer	Ove ARUP & Partners
Total no of apartments	86
Total project cost	Value - £500m (approx)
PT system	Ground floor & beams; Bonded Multi-strand system (19 x 15.7mm) & Mono-strand (15.7mm) For superstructure Bonded Flat Duct Mono-strand system (12.9mm)
Scope of PT	Ground floor - 15.7mm <ul style="list-style-type: none">• Multi-strand beams – 17 in total (2 x 19 strand tendons per beam)• Mono-strand Superstructure – 12.9mm <ul style="list-style-type: none">• Pavilion A – Level 1-10• Pavilion B – Level 1-12• Pavilion C – Level 1-14• Pavilion D – Level 1-12
PT Tonnage	Ground floor – 10MT Superstructure – 225MT
Key Facts	<ul style="list-style-type: none">• 70,000m³ of Excavation;• 21,000m³ Concrete;• 4300MT steel;

One Hyde Park

The most luxurious residential apartments in London, One Hyde Park is created on the site of the former 1950's building Bowater House in Knightsbridge.

Designed by architect Richard Rogers, the development consists of eighty-six apartments and three exclusive boutiques within four pavilions of between ten and fourteen storeys above a four level basement.

The feature elements of structural steelwork and architectural quality precast concrete make this project stand out as a rare development.

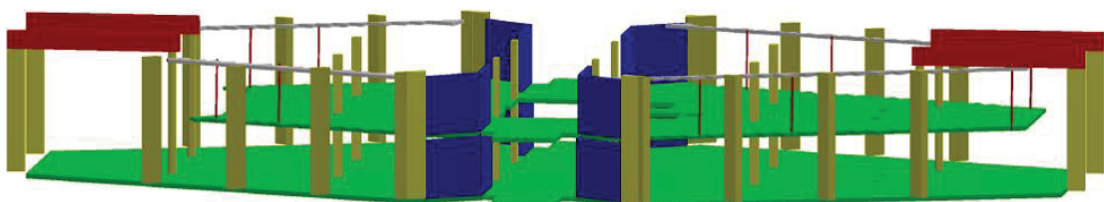


Post-tensioning

A total of 235 tonnes of post-tensioning strand was installed in this iconic structure over the course of 56 weeks. Multiple post-tensioning (PT) applications were utilised to achieve an efficiency of design, materials and labour.

Ground Floor

The ground floor is a mixture of reinforced and post-tensioned beams and slabs using bonded (15.7mm) PT. PT transfer beams were located at ground level and are accommodated within the B1 storey height. The use of 1200mm deep x 2400mm wide transfer beams with multi-strand PT simultaneously minimised the depth of the beams hence reducing the depth of excavation in the basement. The PT arrangement was required to reconcile the trapezoidal superstructure column layout with the substructure column grid. (Refer SF-PTA-2009-SK-1). Each beam contained two 19strand 15.7mm tendons.



Typical Floor Slabs

Both conventionally reinforced and PT options were evaluated. The PT slabs were considered more suitable on the basis of efficiency under the high superimposed dead loads from heavy-weight partitions and luxury finishes, reduction in building mass and material and for speed of construction. The PT solution provided the advantage of structural efficiency, spans (greater than 8.5metre), whilst maximising the floor to floor height within apartments given the planning constraints on the overall building height. (Refer SF-PTA-2009-SK-2, 3 and 4).

Various vibration sources such as London Underground's (within the basement) Piccadilly line, Edinburgh traffic Gate, HGV Lift and vehicle lift structure made acoustics one of the key factors in determining slab thickness. This coupled with the floor finishes and ceiling build-up meant a minimum slab thickness of 280mm for roof slabs and 250mm for other superstructure levels were selected to provide the most efficient solution when evaluated in relation to vibration, acoustics, punching shear, stair and service penetrations.



Penthouse and Roof

A consistent slab thickness was used on typical floors of all Pavilions in order to maintain repetition of detail in structure, façade, formwork and finishes. The geometry of the upper penthouse level comprises triangular recesses on the long side to give saw-tooth slab edges. Hangers were provided from the roof slab above to support the re-entrant corners and assist the edge columns with slab support. (Refer SF-PTA-2009-SK-6)

The roof slab is a post-tensioned slab spanning between internal precast concrete upstand beam edge beams and columns. Whilst incorporating these precast elements the roof slab design needed to control crack widths to remain watertight whilst accommodating the gantry loadings onto the precast.

The slab depth increased at roof level from 250mm to 280mm in order to accommodate the loads imposed on the slab by the architectural beams, cleaning cradle and the additional loads imposed through the hangers at the perimeter. The mezzanine slab of the penthouse level on each pavilion was suspended from the roof slab by steel rod hangers, where slab edges are irregular and recessed from upper columns. Furthermore, this slab was able to accommodate a series of smaller penetrations and larger openings at mid span on both ends of the slab. (Refer SF-PTA-2009-SK-7, 8 and 9)



Design Challenges

The PT layout needed to be co-ordinated with façade and glazing works, precast columns, precast spandrels, mezzanine hangers and structural steel items as well as late alterations to site logistics and construction sequence.

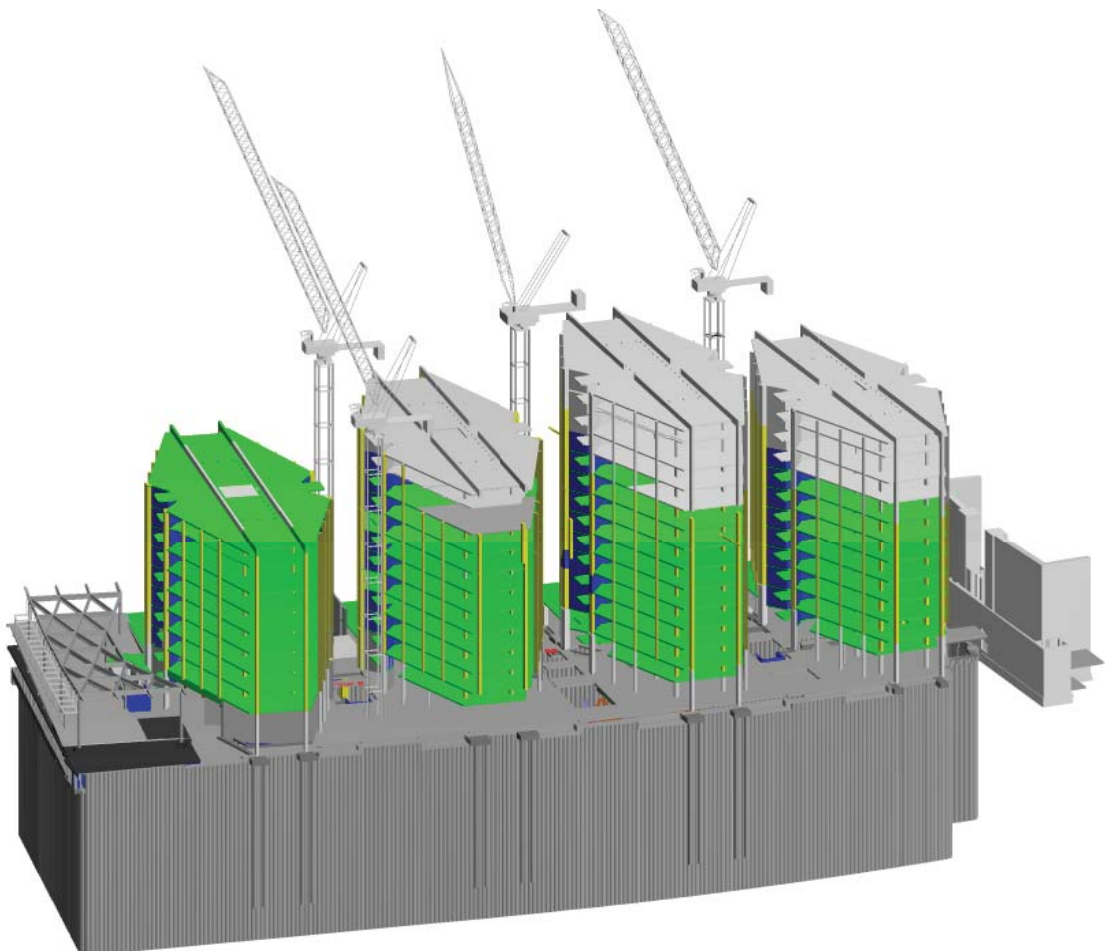
A late request by Transport for London (TFL) for an area of the site to be used for traffic management during their roadwork's at the busy Knightsbridge intersection required the end thirds of two pavilions to be delayed behind the rest of the structure. Hence an additional pour strip was introduced along the southern edge of Pavilion's B and C (Refer SF-PTA-2009-SK-2, 3 and 4).

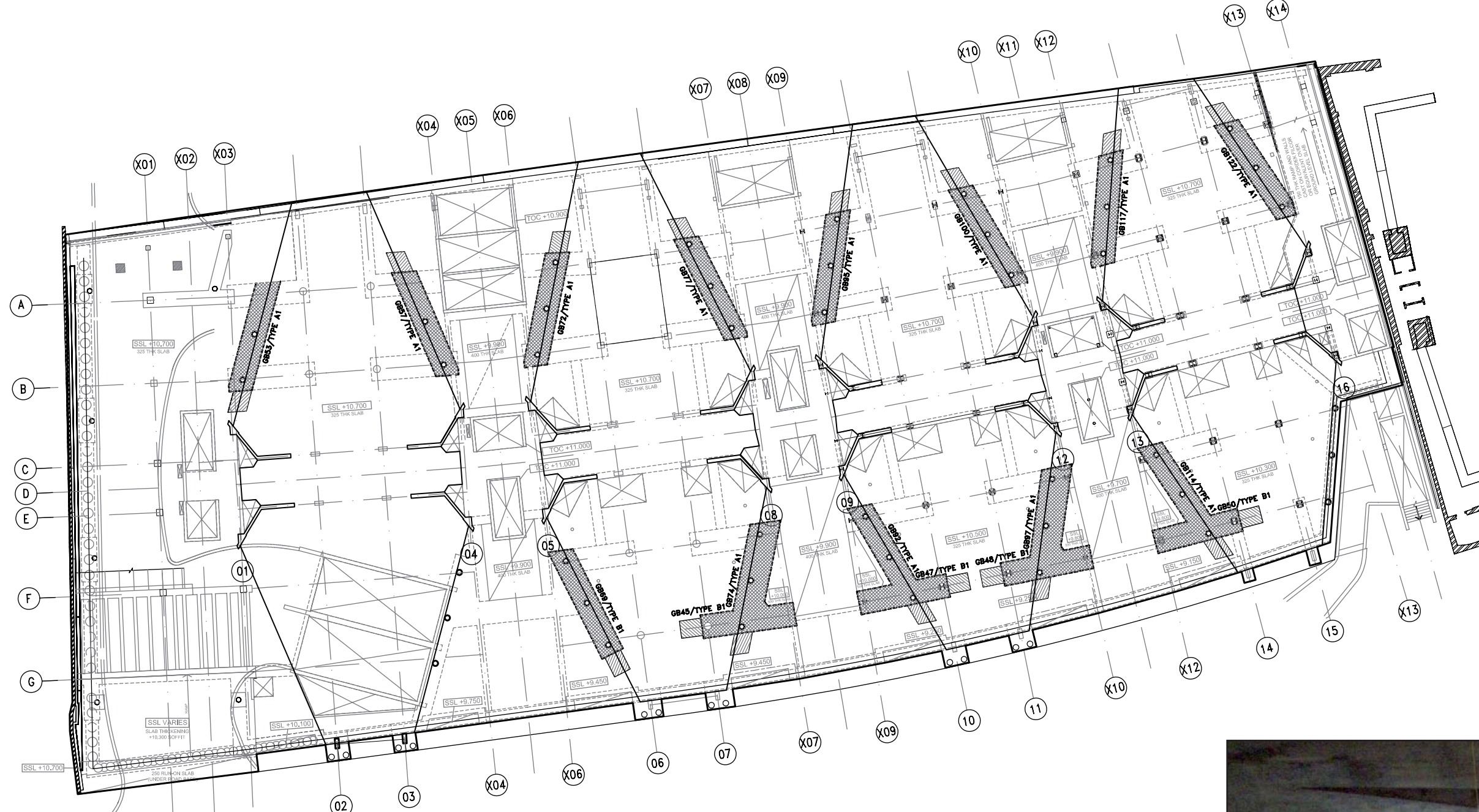
An innovation on this project was incorporation of the steel transfer truss with the PT slabs. On Pavilion A level 2 a steel transfer truss was sought as best solution to overcome column restrictions imposed by the reception drop off space and access to the basement parking lift. The slab was designed as post tensioned which required the tendons to pass through the steel truss. The setting out for the PT and reinforcement were co-ordinated with the truss fabricator and voids were then formed in the truss for the PT ducts to pass through fabrication. (Refer SF-PTA-2009-SK-5)

Feature steelwork was also used to help provide stability to the pavilions. The stability frames as shown on section 21 of sketch SF-PTA-2009-SK-2 have been proportioned on a two storey module to align with the façade. The stability system relies on the coupling of steel frames with the internal reinforced concrete shear walls braced with the PT slabs.

Sustainability

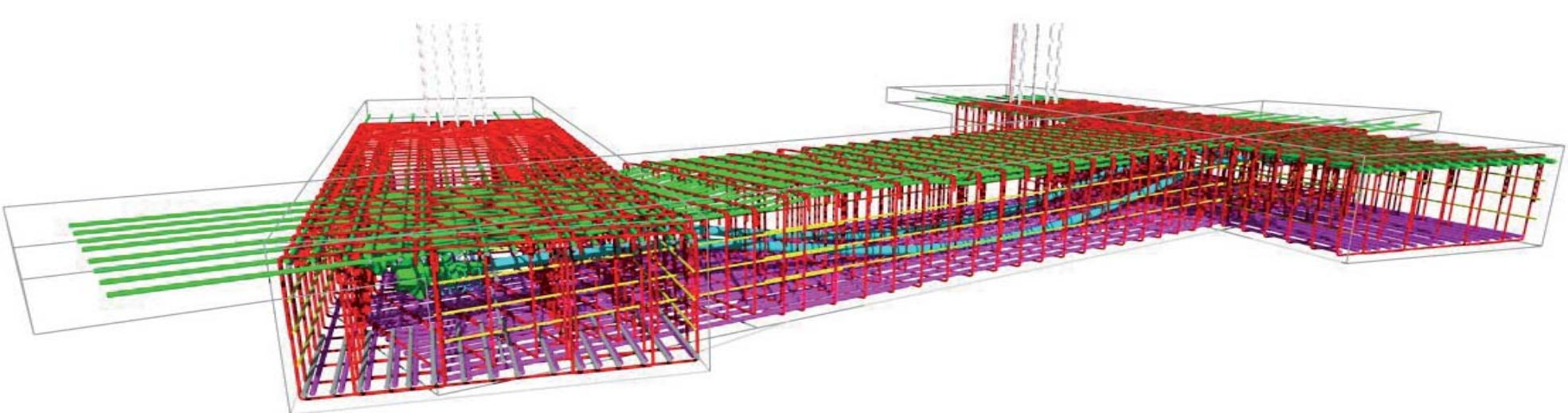
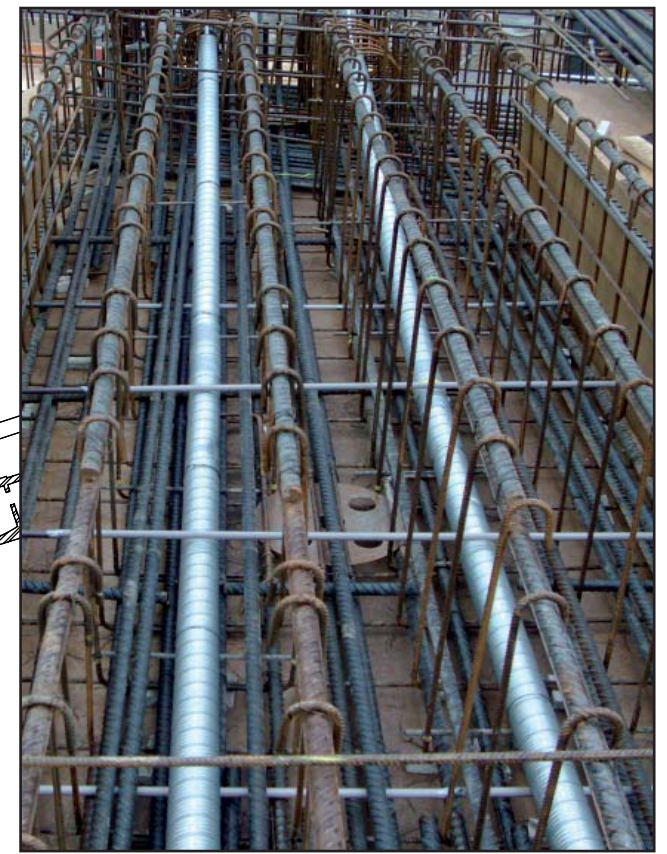
All the building materials used on site conform to 'Ecohomes 2006 – The environmental rating for homes'.





GROUND FLOOR TRANSFER PT BEAMS CARRY THE SUPERSTRUCTURE LOAD. THESE BEAMS COMPRISE 19s-0.6" MULTISTRAND TENDONS.

TEMPORARY OPENING FOR STRESSING ACCESS.



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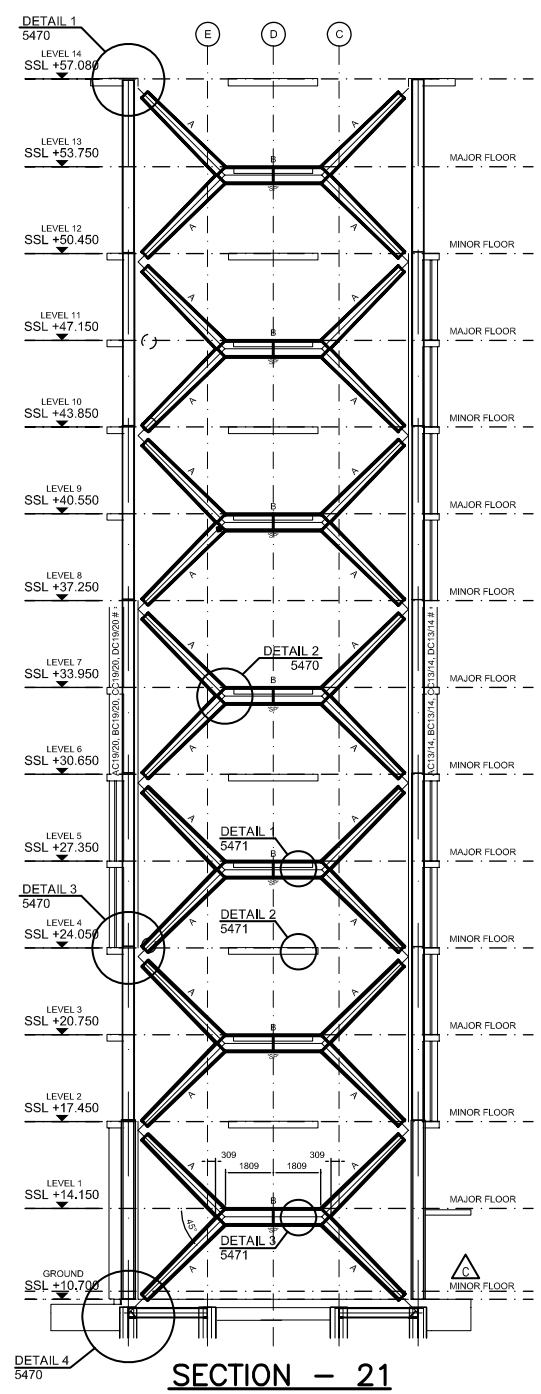
POUR STRIP ORIGINALLY LOCATED BETWEEN GL C-E

Post Tensioning Plan

SLAB POST TENSIONED TO SUIT AN OVERALL SLAB DEPTH OF 250mm.

POUR STRIP RELOCATED DUE TO ACCESS CONSTRAINTS IMPOSED BY TFL

MAJOR FLOORS SUPPORTED BY STABILITY FRAME. MINOR FLOORS HUNG FROM MAJOR FLOORS USING HANGERS. SEE SECTION 21

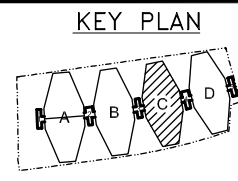


- POST TENSIONING NOTES.**
- FOR ALL GENERAL AND CONSTRUCTION NOTES, AND ALL ANTIBURST REINFORCEMENT DETAILS REFER TO DRAWING No. 2350_SW_AL_GN_0001.
 - FOR ANTIBURST REINFORCEMENT FOR POST TENSIONING AT THIS LEVEL REFER TO THE FOLLOWING BENDING SCHEDULE.
SCHEDULE No. 01
DRAWING No. 2350_PC_03_PT_0300
CONTRACT No. F1922
NUMBER OF ANTIBURST HELIX TO BE SCHEDULED (Insitu Concrete Only)
(PANNED LIVE END ANTIBURST REPEAT ALL AS TYPICAL LIVE END)
2 + 3 Strand
LIVE ENDS - 0 Bar Mark "500"
DEAD ENDS - 0
4 + 5 Strand
LIVE ENDS - 60 Bar Mark "501"
DEAD ENDS - 70
PANNED END (Trimmer Bars) - 10 Bar Marks "502, 503, 504"
 - POST TENSIONING ANTIBURST REINFORCEMENT NOT SHOWN ON PLAN. REFER TO TYPICAL DETAILS ON DRAWING No. 2350_SW_AL_GN_0001.

Bar Chair Quantities			
Chair Height	No. Off	Chair Height	No. Off
35	43	110	82
40	36	100	52
45	32	115	24
50	24	120	42
55	77	125	30
60	40	130	34
65	28	140	6
70	34	145	30
75	48	150	16
80	36	155	84
85	37	160	16
90	38	165	2
95	18	170	14
		175	66



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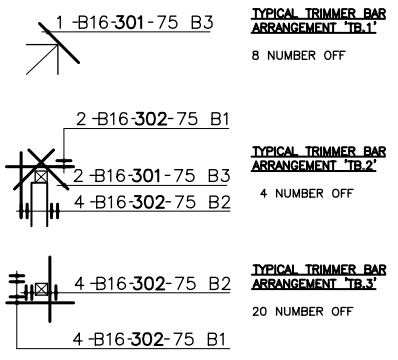
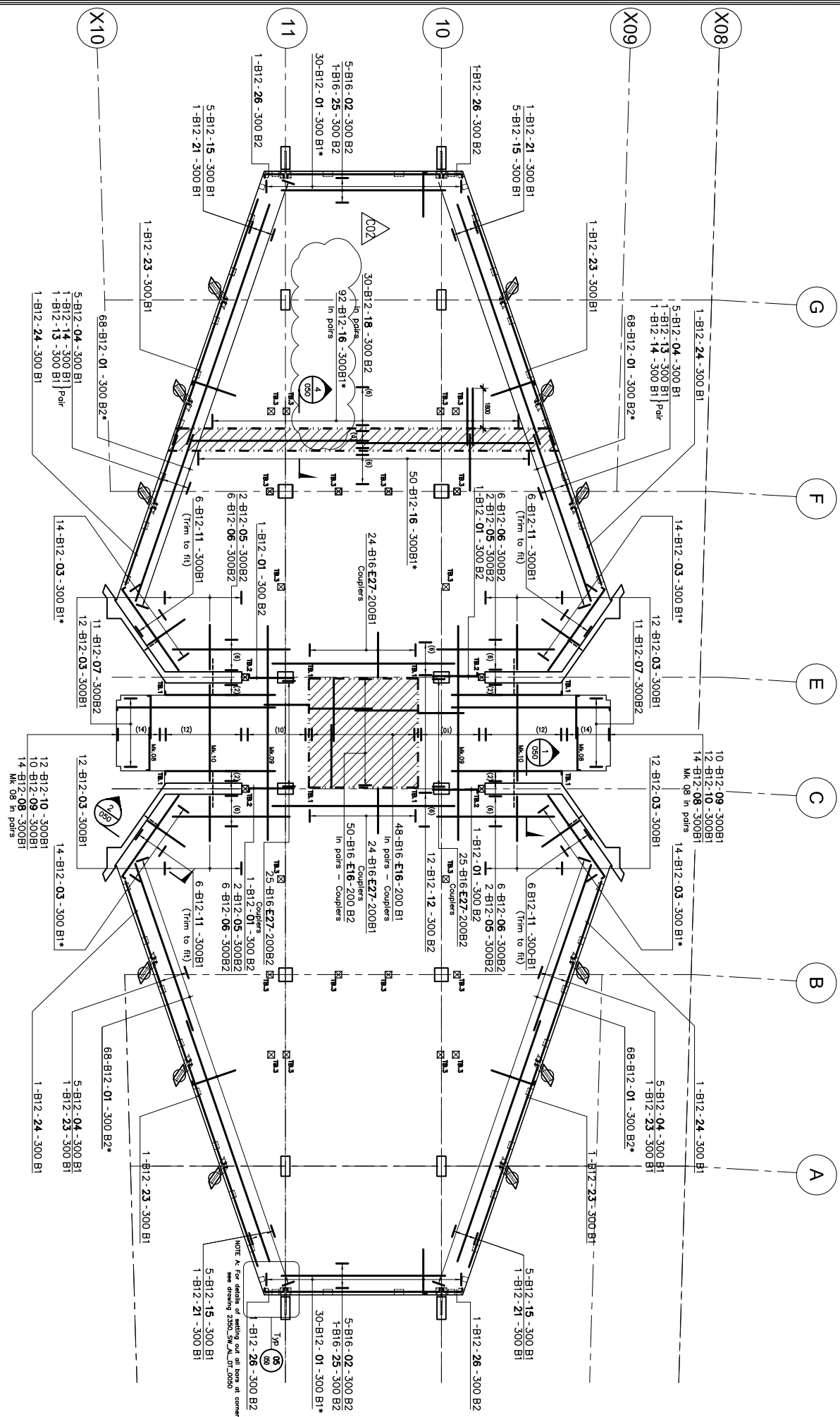
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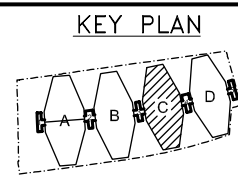
Project
**One Hyde Park
Knightsbridge**

Drawing
**Post Tensioning Plan
Pavilion C, Level 3
Pours 1 & 2**

SF-PTA-2009-SK-2



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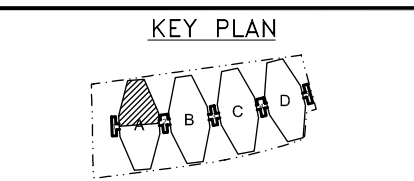
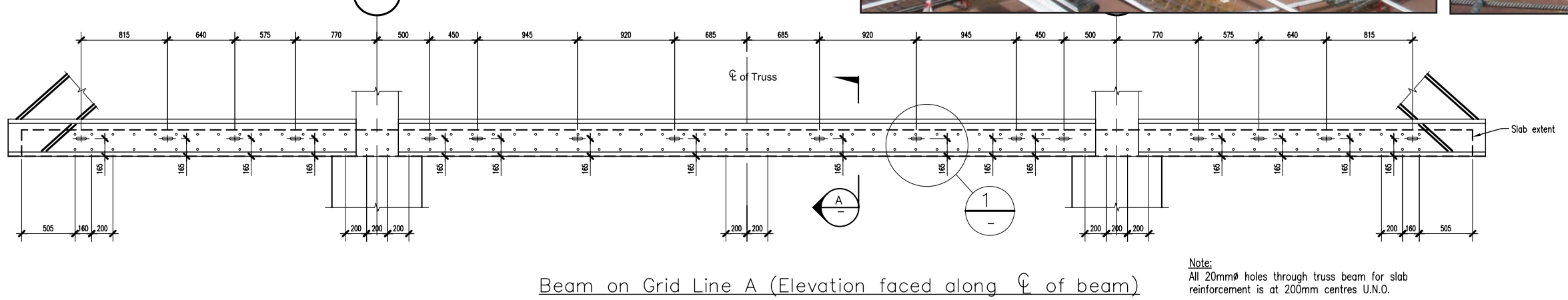
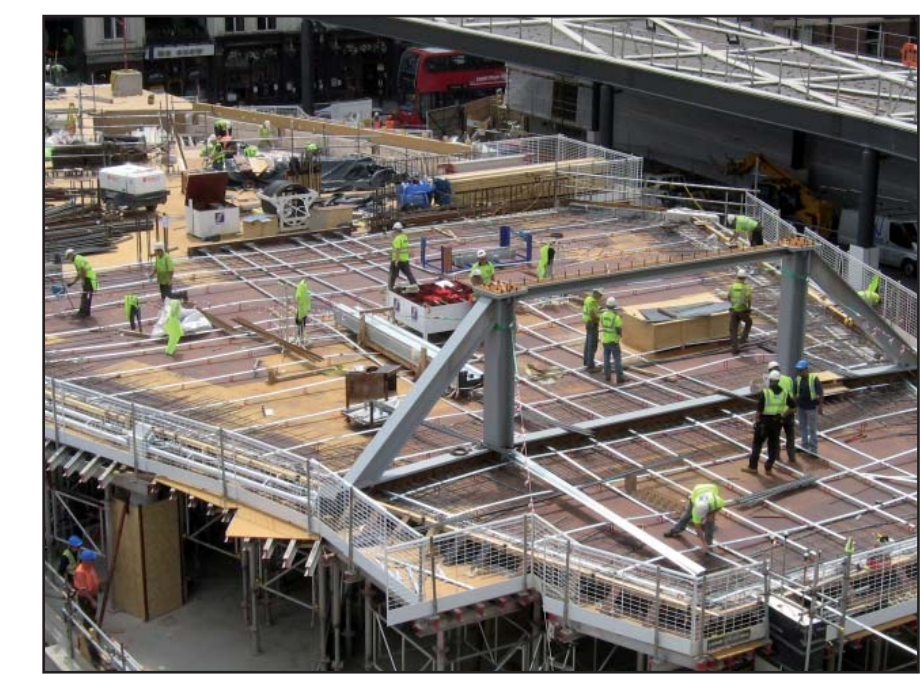
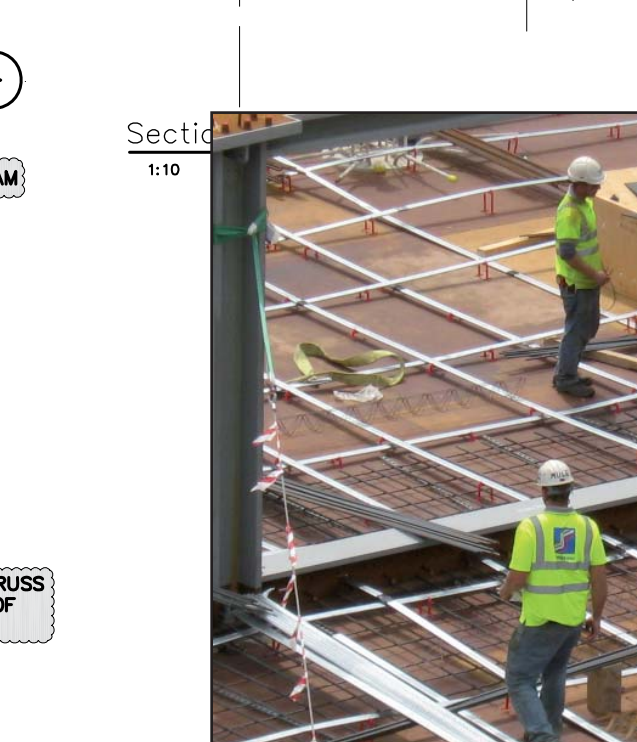
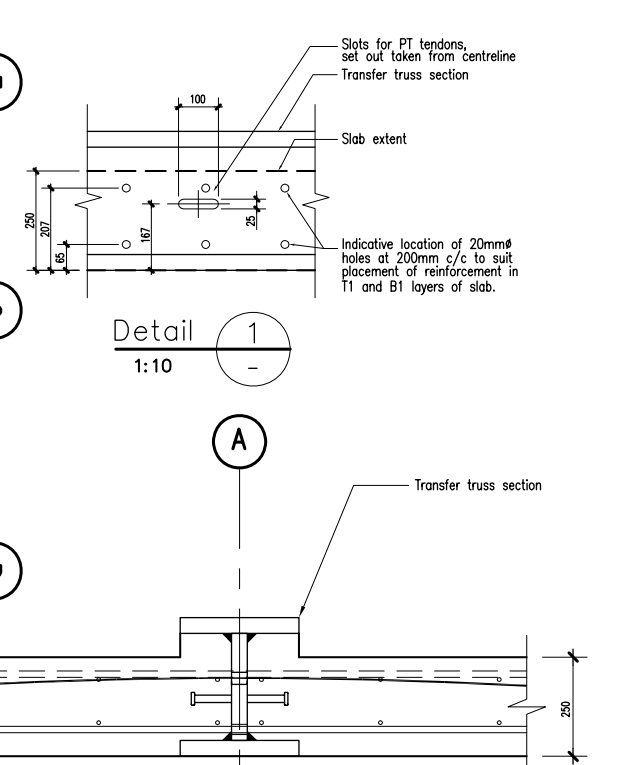
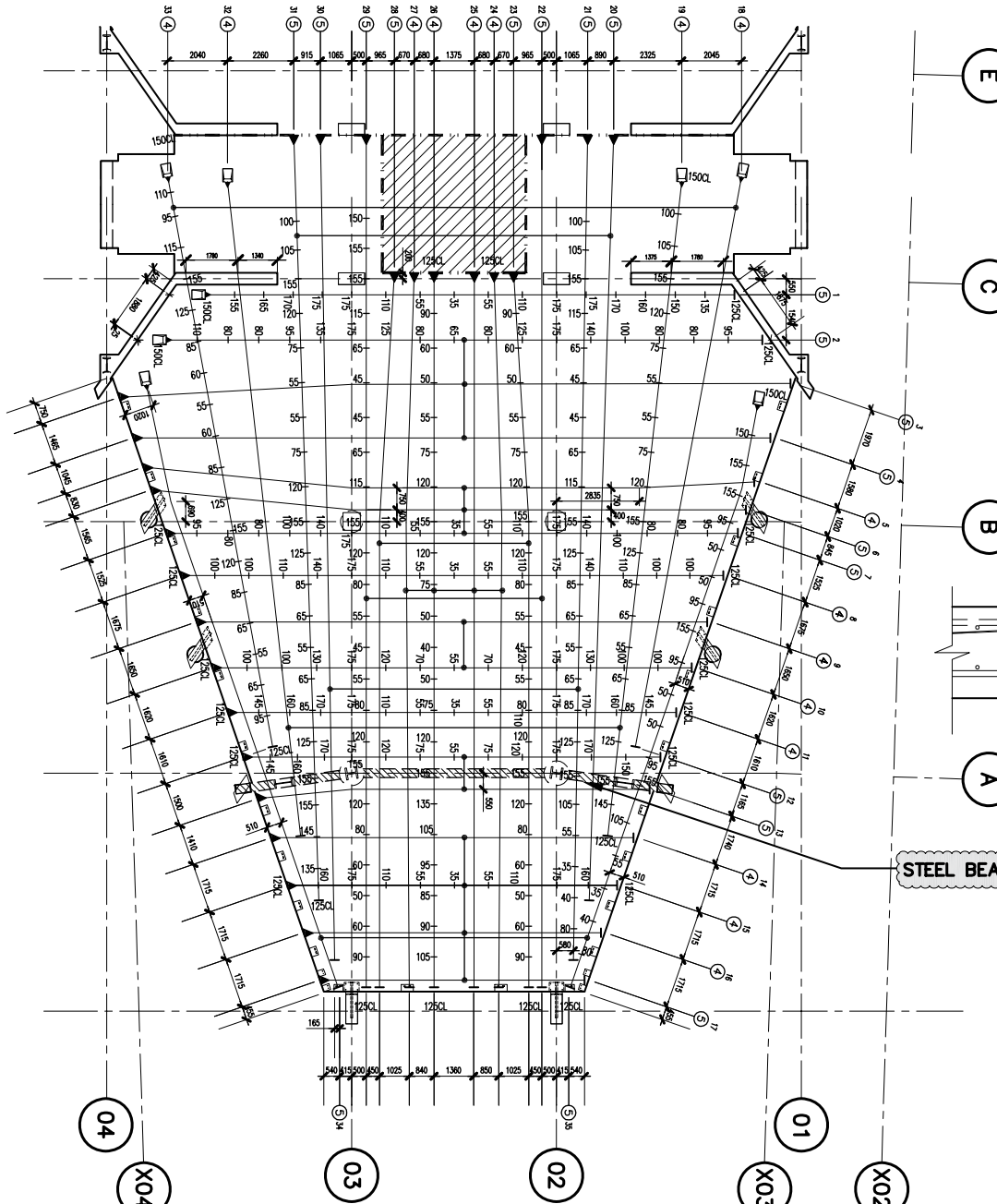
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Project
**One Hyde Park
Knightsbridge**

Drawing
**Bottom Reinforcement Plan
Pavilion C, Level 3
Pours 1 & 2**

SF-PTA-2009-SK-3



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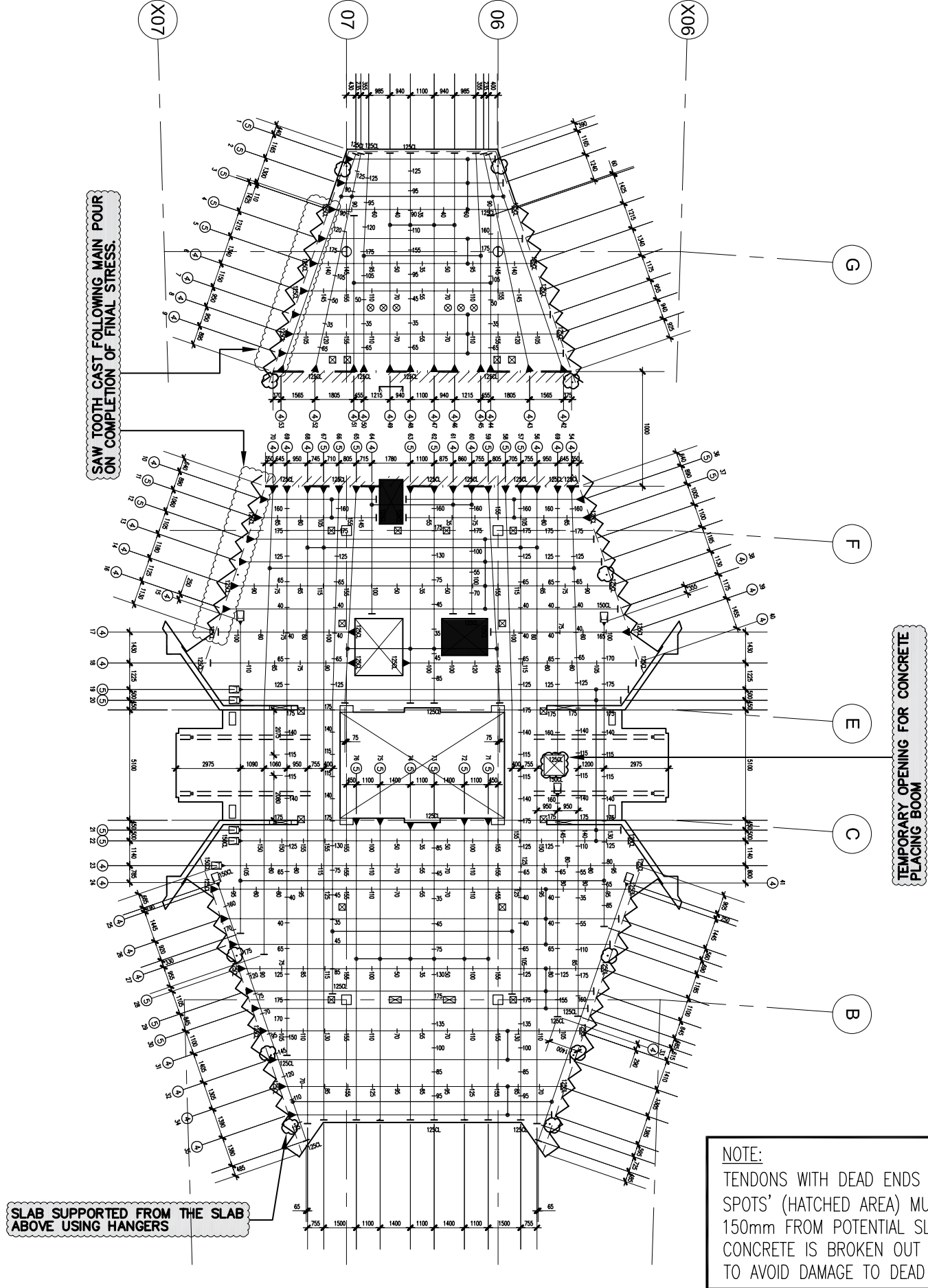
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Project
**One Hyde Park
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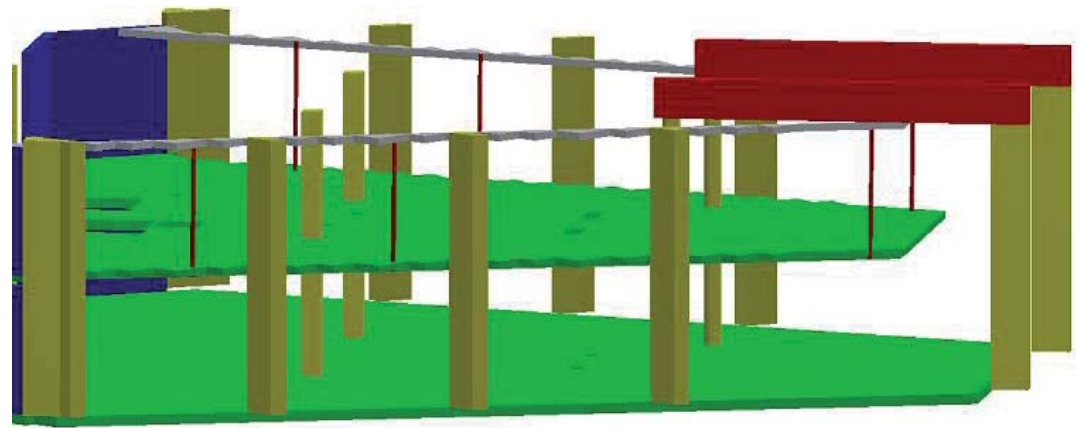
Drawing
**Post Tensioning Plan
Pavilion A, Level 2
Pour 1**

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SF-PTA-2009-SK-5



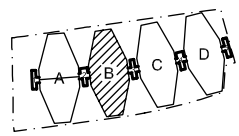
Post Tensioning Plan

SLAB POST TENSIONED TO SUIT AN OVERALL SLAB DEPTH OF 250mm.



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KEY PLAN



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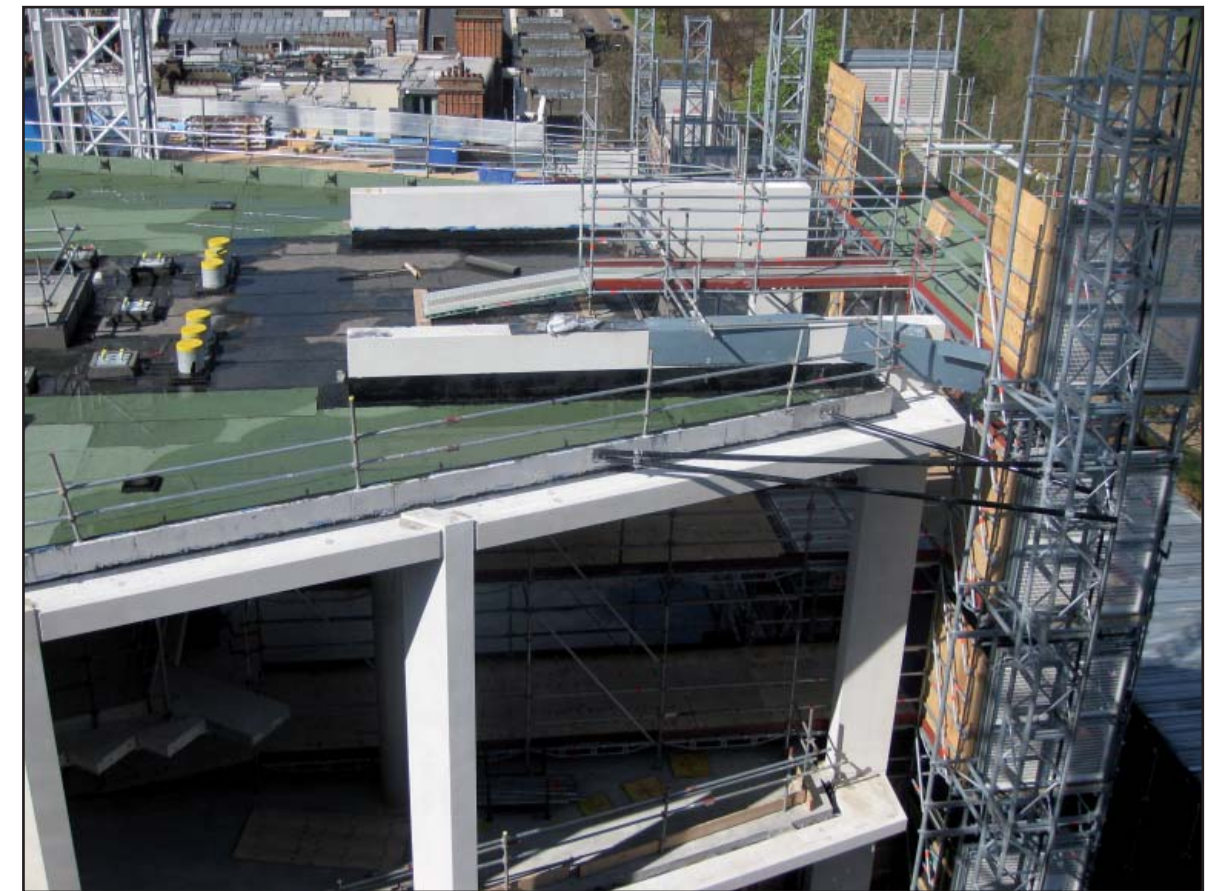
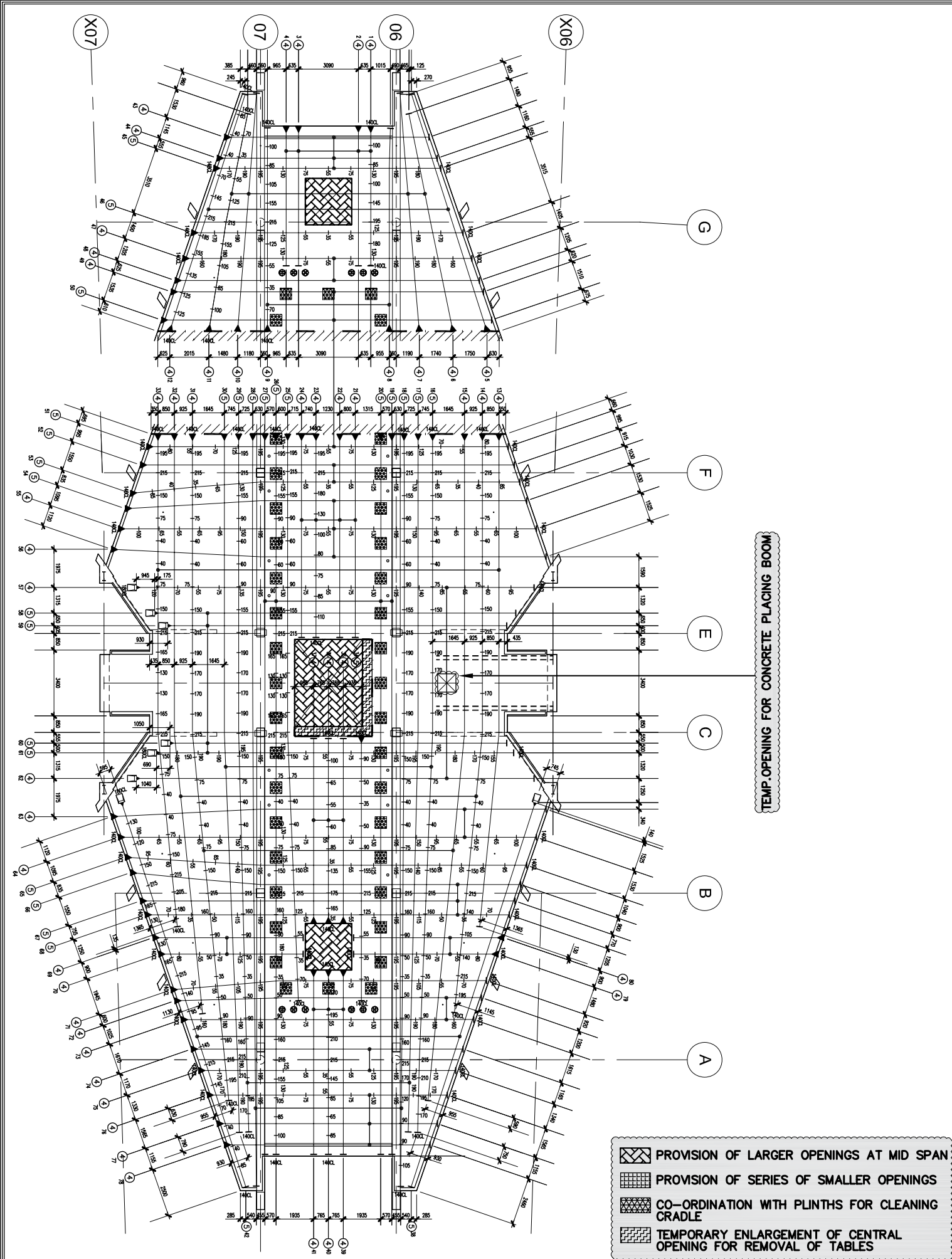
Project

*One Hyde Park
Knightsbridge*

Drawing

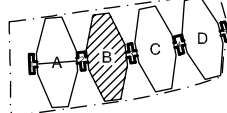
*Post Tensioning Plan
Pavilion B, Level 11
Pours 1 & 2*

SF-PTA-2009-SK-6



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KEY PLAN



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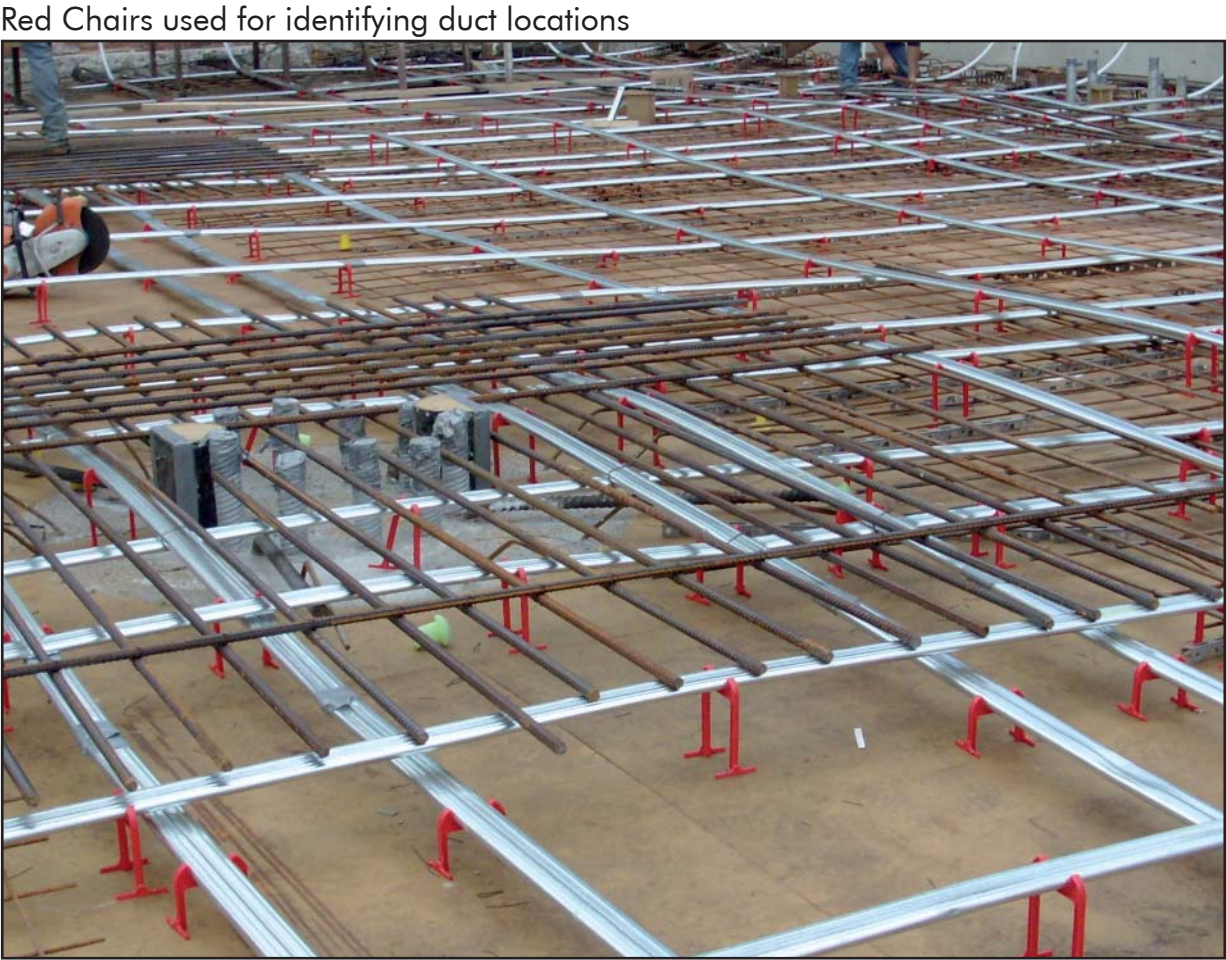
Project

*One Hyde Park
Knightsbridge*

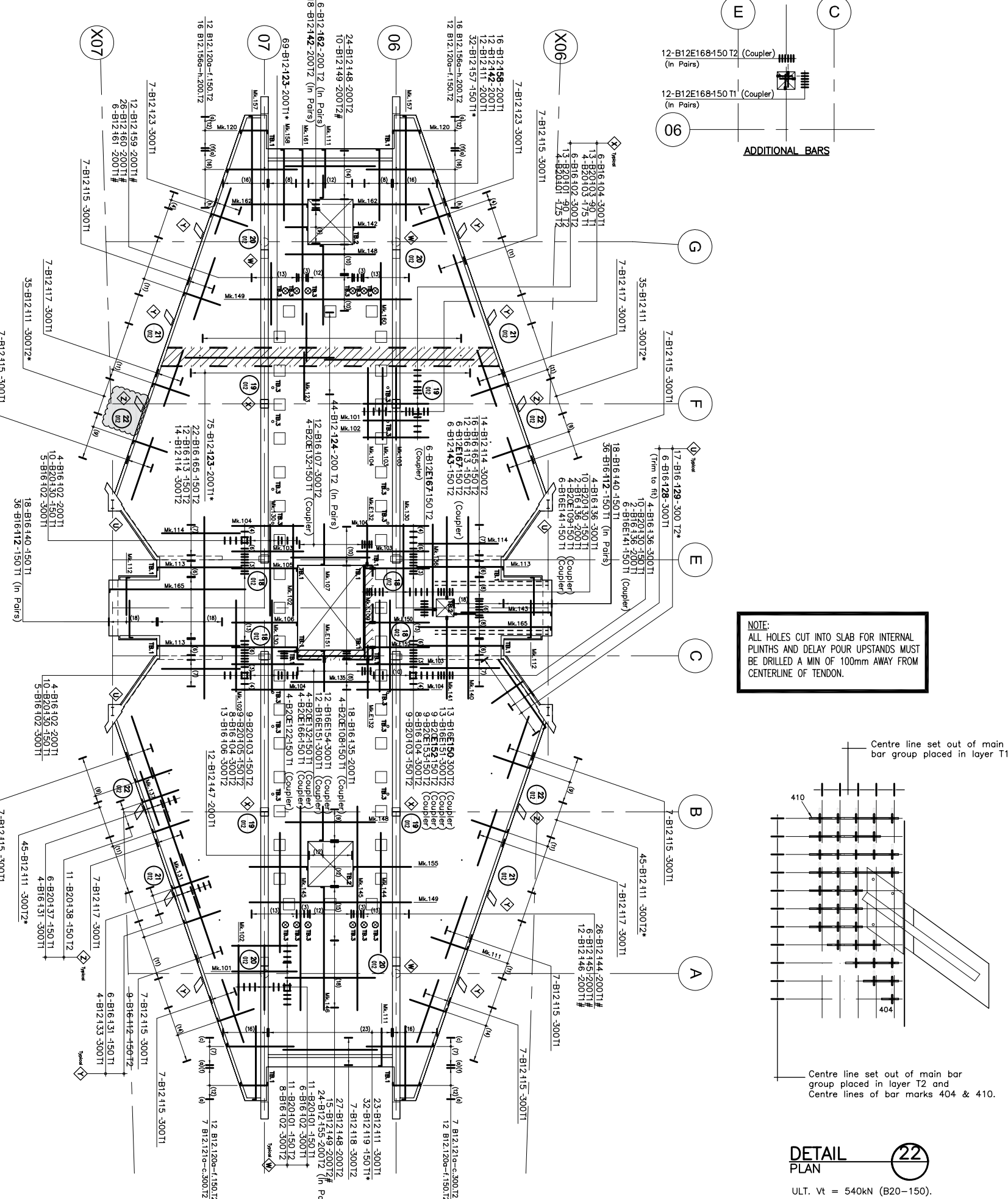
Drawing

*Post Tensioning Plan
Pavilion B, Level 12
Pours 1 & 2*

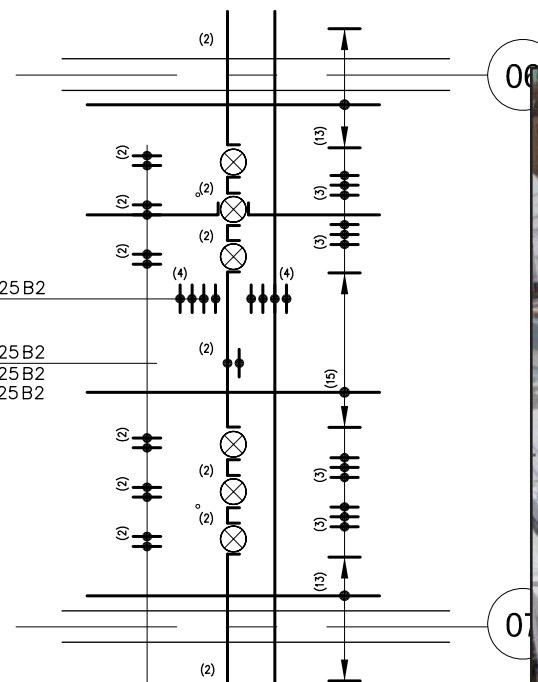
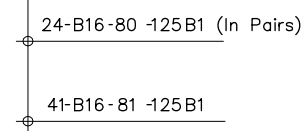
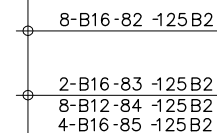
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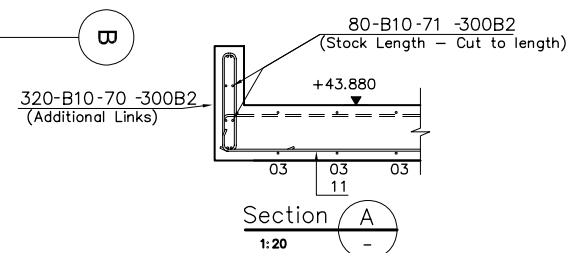
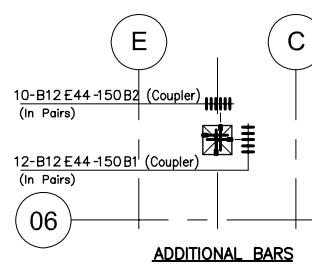
Red Chairs used for identifying duct locations



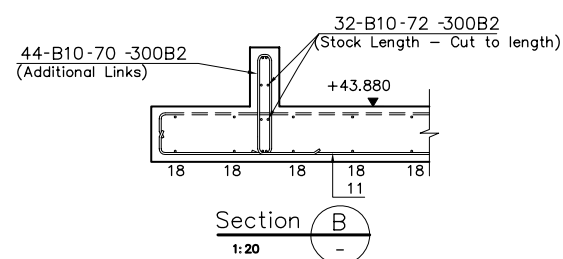
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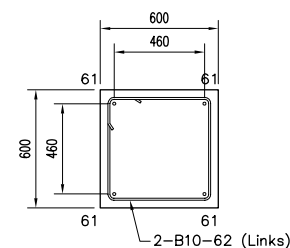
TYPICAL DETAIL V
ADDITIONAL BARS
SCALE - 1:50



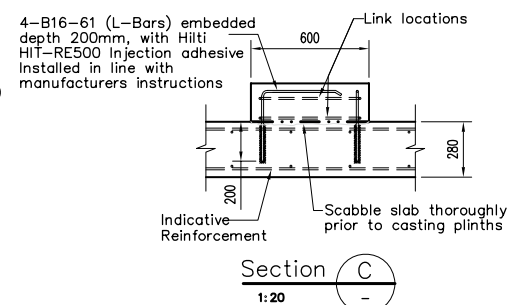
TYPICAL EDGE UPSTAND
ADDITIONAL BARS



TYPICAL 200 x 300 INTERNAL UPSTAND
ADDITIONAL BARS



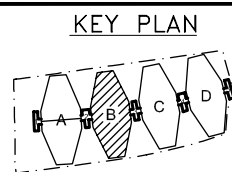
TYPICAL 600x600
INTERNAL PLINTH PLAN
ADDITIONAL BARS
SCALE 1:20



TYPICAL SECTION THROUGH INTERNAL PLINTH
ADDITIONAL BARS



Post-tensioned roof slab can accommodate any services

Project Consultant

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Project

One Hyde Park
Knightsbridge

Drawing

Bottom Reinforcement Plan
Pavilion B, Level 12
Pours 1 & 2

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SF-PTA-2009-SK-9